Removal of Remazol Red from Textile Waste Water Using Treated Sawdust - An Effective Way of Effluent Treatment

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Abstract

Activated carbon prepared from sawdust is endeavored as adsorbent for the removal of reactive dye, namely Remazol Red (RR) from aqueous media. The adsorption of RR has been studied onto activated sawdust at various particle size, adsorbent dose, temperature and pH values. The adsorptions of the above mentioned dye were designed for the Langmuir and Freundlich Isotherms. Pseudo first and second order kinetic models were used to calculate the amount adsorbed at equilibrium (q_e). The calculated values of q_e for pseudo-second order equation were found to be in good agreement with those of experimental values. The monolayer capacity (q_m) for treated sawdust (8.00 mg g⁻¹) is greater than commercial charcoal (0.074 mg g⁻¹). It is established that treated sawdust has been used as a better adsorbent for the removal of RR as compared to commercial charcoal. This process may eventually be used to get industrial waste free purified water.

Key words: Sawdust, Remazol Red, Adsorption Isotherm, Adsorption Kinetics.

Introduction

Industrial effluents are one of the major pollutants of water. Many dyes are carcinogenic and affect the life of aquatic organisms (Baughman et al., 1998; Hassan et al., 2009). Removal of azo dyes from the effluent generated by textile industries is rather difficult. Azo dyes represent a major class of synthetic colorants that are both mutagenic and carcinogenic (Waghmode et al., 2012). Reactive dyes are extensively used in textile industry and due to their large size they have high affinity to bind with cellulosic fiber. The worldwide annual growth rates of reactive dyes are four times as much as for conventional dyes (Zollinger, 2003). Vinyl sulfone dyes are a class of reactive dyes effectively used for cotton, silk and wool. They are also known as remazol dyes after the trademarked name under which they were first introduced. Vinyl sulfone dyes are less reactive than other dyes and therefore major part of these dyes remains in dyeing bath or drained off as industrial effluents. It has been reported that up to 30% of the used dyestuff remains in the spent dye-bath after the dying process (Ozacar et al., 2005). Presence of such dyes in effluents causes a lot of pollution in water. Various challenges have been made to remove these harmful dyes from industrial wastes (Ho et al., 2005; Mohanty et al. 2006; Sousa et al., 2012).

Adsorption is one of the cheapest and most effective techniques (Cotoruelo *et al.*, 2007; Dee *et al.*, 2006). Different adsorbents are used for the removal of dyes from aqueous solutions such as alumina, crushed bricks, peat, sand, charcoal bentonite, silica, apricot etc (Hu *et al.*, 2006; Jain *et al.*, 2009; Mon, 2004; Senthilkumaa *et al.*, 2006). The most widely used adsorbent for the removal of dyes are charcoal prepared from saw dust which is inexpensive and easily available. Therefore, the interest is growing to find out an alternative adsorbent to commercial charcoal.

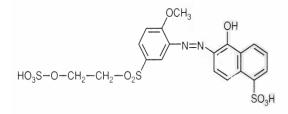


Figure 1. Structure of Remazol Red.

The objective of this work is to study the feasibility of activated sawdust as alternate adsorbents to commercial charcoal (Ahmadpour *et al.*, 1997; Arivoli *et al.*, 2010) for the removal of Remazol Red (RR) (Figure 1). The adsorption results of RR onto saw dust are also compared with that of commercial charcoal.

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Materials and Methods

Preparation of activated charcoal: There are two different methods for the preparation of activated carbon: physical activation and chemical activation (Ho *et al.*, 2005). In comparison to physical activation, chemical activation provides a number of advantages. The process of dye removal was applied in batch mode. Adsorption experiments were performed by suspending sawdust in the effluent and analyzing the supernatant by spectroscopic method.

Sawdust (Shegun, Tectona grandis) was collected from nearby Sawmill (Rampura, Dhaka, Bangladesh). This was washed with double distilled water to remove water-soluble impurities and surface-adhered particles. Then the adsorbent was oven-dried at 60°C to remove the moisture and other volatile impurities. Then, part of the dried sawdust was soaked in concentrated H₂SO₄ in an amount sufficient to cover the material completely, agitated at 120 rpm in a shaking incubator for 30 min, and then left for 2h. After being mixed, the slurry was subjected to vacuum-drying at 100° C for 24 h. Chemical activation of the sawdust was performed with ZnC12. Ten grams of sawdust was mixed well with 100 ml of 10% of ZnC1₂ solution. The mixing was performed at 50° C for 1 h. After mixing, the slurry was subjected to vacuumdrying at 100° C for 24 h (Mohanty et al., 2006; Ahmadpour et al., 1997).

The resulting impregnated solids was placed in a stainless steel tubular reactor and heated (5° C min⁻¹) to a temperature of 300° C under nitrogen flow at a rate of 150 cm³ min⁻¹ at STP for 1 h. Nitrogen entering the reactor was first heated to 250-300°C in a preheater. The products were washed sequentially with 0.5 M HCI, hot water and finally with cold distilled water to remove residual organic and mineral materials and then dried at 110° C. In all experiments, the heating rate and nitrogen flow were kept constant.

Preparation of dye solution: Remazol Red (RR) was used in the experiment. It is a reactive dye supplied by Dye Star Ltd., Dhaka, Bangladesh. This dye form covalent bond with the fiber, usually cotton, although it used to a small extent on wool and nylon. This class of dyes first introduced commercially in 1956, made it possible to achieve extremely high washing fastness properties by relatively simple dyeing methods. A stock solution of 1000 ppm RR was prepared by dissolving appropriate amount of dye in water. The required concentration was prepared for the various steps of the investigation by dilution.

Study of batch adsorption process: Equilibrium isotherms for adsorption onto the selected carbons determined by using 1 g of adsorbent per 50 ml of aqueous solution for initial dye concentrations in the range of 50-200 ppm. For these experiments, the bottles were shaken at constant temperature (25°C) and agitation speed (120 rpm), for the minimum contact time required to attain as determined from the kinetic equilibrium, measurements. The effectiveness of the treatment was evaluated by measuring concentration by UV-Visible spectroscopic method at 541.5 nm.

The influence of pH was studied by adjusting the reaction mixture to different initial pH values and analyzing the residual color at the equilibrium contact time. The pH values were adjusted with dilute sulfuric acid and sodium hydroxide solutions. Then the percentage of dye removal was calculated by,

The amount of dye adsorbed onto the activated carbons, $q_e (mg/g)$, was calculated according to:

where C_0 and C_e are the initial and the final dye concentrations (mg/l), respectively, and W is the amount of adsorbent (g), V is the volume of the solution (L).

Results and Discussion

The physical properties of treated sawdust: The physical properties of the treated sawdust have been shown in the Table 1. From the table it is found that the BET surface area (Rabolli *et al.*, 2010) is 5.69 m²/g and the average pore diameter is 99.60 A⁰. The point of zero charge (pzc) of the above mentioned adsorbent is 5.5.

Optimization of contact time: The contact time between dye and adsorbent is of significant importance in waste water treatment by adsorption methods. A rapid removal of pollutants and establishment of equilibrium in a short period signifies the efficacy of the adsorbent. The effect of shaking time for the adsorption of dye onto charcoal prepared from sawdust was determined at 25°C. The fixed concentration of RR was shaken after adding 1g of adsorbent in each time. Color removal was rapid at initial stage but decreased with the increase of time (Fig. 2). Initially rapid increase was due to the presence of large number of vacant site and with the passage of time, number of active sites decreased which were responsible for the reduction of adsorption rate. The optimum contact time was observed 12 hours for all the adsorbents.

Table 1. Physical properties of treated sawdust.

Properties	value
Particle size (µm)	<140
BET surface area (m ² /g)	5.69
Average pore diameter (A ⁰)	99.60
Micro pore volume(cc/g)	0.014
Micro pore area (m ² /g)	2.37
Bulk density (g/ml)	0.84
pzc	5.5

Optimization of adsorbent amount: For optimizing the amount of adsorbents, experiments were performed using 50 ml aqueous solution of RR and was shaken for 120 minutes after adding different amount of adsorbents (0.5-3.0 g). Absorbance of the filtrate was noted using spectrophotometer at λ_{max} of the dye. It was observed that adsorption of dye increased with the increase of the amount of adsorbents and then attained constant value at equilibrium (Fig. 3). The optimum amount was found to be 1.0g which was used for all subsequent adsorption studies.

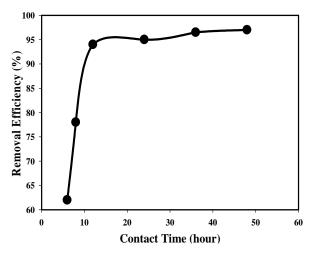


Figure 2. Effect of contact time on the removal of RR. Particle size: 140μm; Adsorbent amount: 1.0 g; Initial conc.: 50 mg/l; Initial volume: 50 ml; pH: 7.0; Temp.: 25⁰C.

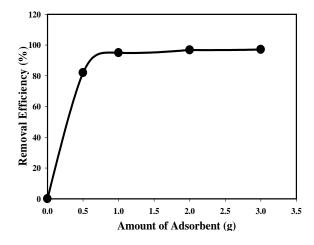


Figure 3. Effect of adsorbent amount on the removal of RR. Particle size: 140 μm; Initial concentration: 50 mg/l; Initial volume: 50 ml; pH: 7.0; Contact time: 12 hours; Temp.: 25⁰C.

Influence of initial pH: Hydrogen and hydroxy1 ions are usually adsorbed quite strongly on the surface of the adsorbents due to their smaller size as compared to the dye molecules and therefore adsorption of other ions is affected by pH of the solution. The pH primarily affects the degree of ionization of the dye as well as surface properties of the adsorbents. Adsorption of RR decreased with increase in pH (Figure 3). This can be explained on the basis that positively charged surface is formed on the adsorbents at lower pH due to adsorption of hydrogen ions on the surface of adsorbents.

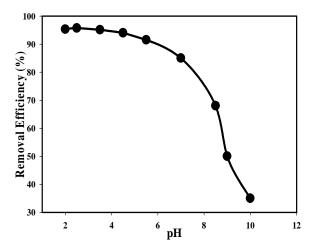


Figure 3. Effect of pH on the adsorption capacity of saw dust for Remazol red at 25^oC.

It has been reported that the positively charged ions prefer to adsorb at higher pH value and negatively charged ions prefer lower pH. As pH of the system increases, number of positively charged site on the surface of adsorbents decreases. As the dye is in dissociated form the anion (Equation 3) and as a result adsorption of dye decreased at higher pH values.

ASO₂ Na
$$\longleftrightarrow$$
 ASO₂ Na⁺(3)

The decrease in the amount of dye adsorbed on surface of the adsorbents with increase in pH is in good agreement with the data reported earlier (Ahmadpour et al., 1997)

Adsorption isotherms: The adsorption isotherms of RR on sawdust were found to be L-type in each case (Ho et al., 2005). The initial sharp rise in the degree of adsorption with increasing dye concentration is due to the availability of higher adsorption sites on the surface of the adsorbents. When the concentration of dye solution increases, adsorption sites are decreased. As a result, the dye molecules find difficulty to access the remaining vacant surface. Adsorption of RR is found to be slightly increased with increase in temperature then remain almost constant (Figure 4). This indicates that desorption process is more favorable at lower temperature and is expected to be an endothermic process.

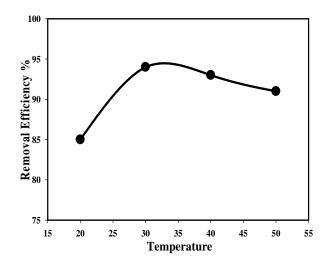


Figure 4. Effect of temperature on the removal of RR. Particle size: 140μm; Adsorbent amount: 1.0 g; Initial conc.: 50 mg/L; Initial volume: 50 ml; pH: 7; Contact time: 12 hours.

Adsorption data for Remazol Red onto activated sawdust was fitted to the linear forms of Freundlich (4) and Langmuir (5) equations

$$\log(q_e) = \frac{1}{n}\log(C_e) + \log(K_F) \dots (4)$$

Where $q_e(mg/g)$ is the amount adsorbed per unit mass of the adsorbent, C_e is the equilibrium concentration, K_F and 1/n are constants, being indicative of the extent of adsorption and degree of non-linearity between solution concentration and amount of dye adsorbed respectively.

From Freundlich plot (Figure 5), the constants K_F and n are calculated from the intercepts and slopes of linear plots of $log(q_e)$ versus $log(C_e)$, respectively and their values are given in Table 2. If n = 1, adsorption is homogeneous and there is no interaction between the adsorbed species. If n < 1, the adsorption is unfavorable and if n > 1, then the adsorption is favorable. In present studies, we have found that n is greater than unity for the given adsorbents which indicates that adsorption is favorable. It has also been reported that the value of K_F gives rough estimation about the degree of adsorption. In the present studies it was observed that the value of K_F for the adsorption of RR onto saw dust (1.71 mgg⁻¹) is greater than those for charcoal (5.91 mg g⁻¹) (Table 2). Greater value of K_F for activated sawdust reflects that it is better adsorbent for the removal of RR than commercial charcoal.

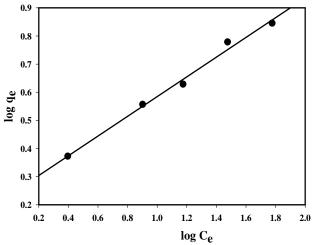


Figure 5. Freundlich isotherms of Remazol Red on saw dust at 25°C.

and commercial charcoal at 25°C.

Table 2. Freundlich parameters for Remazol red on Sawdust

Adsorbents	n	K_{F}	\mathbf{R}^2
Prepared activated saw dust	2.85	1.71	0.991
Commercial activated carbon	1.79	5.91	0.998

Langmuir equation is given as

A plot of C_e/q_e versus C_e should indicate a straight line of slope $1/q_m$ and an intercept of $1/(K_a q_m)$, where C_e is the equilibrium concentration (mg/dm³), q_e is the amount of dye sorbed (mg/g), q_m is q_e for a complete monolayer (mg/g), and K_a is the sorption equilibrium constant (dm³/mg). The essential characteristics of Langmuir eqn. can be expressed in terms of separation factor R_L (Rao *et al.*, 2008),

Where $R_L = 1/(1+K_a.Co)$

- * $R_L > 1$; Unfavorable.
- * $0 < R_L < 1$; Favorable.
- * $R_L = 1$; Linear.

* $R_L = 0$; Irreversible.

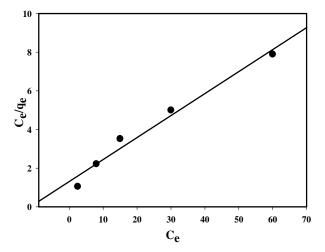


Figure 6. Langmuir isotherms of RemazolRed on sawdust at 25°C.

Table 3. Langmuir parameters and separation factor $R_{\rm L}$ for adsorption of RR on treated sawdust.

Adsorbent	K _a / dm ³ mg ⁻¹	q _m / mgg ⁻¹	R ²	R _L
Prepared activated saw dust	0.105	8.00	0.988	0.045
Commercial activated carbon	7974.8	0.074	0.9448	

Adsorption kinetics: In order to investigate the adsorption processes of Remazol Red onto sawdust two kinetic models were used. Pseudo-first order kinetic equation is given as (Ho et al., 2005):

$$\log (q_e - q_t) = \log q_e - \frac{k_1}{1.202} t \dots (6)$$

Where, q_t is the amount of dye adsorbed at time t (mgg⁻¹), q_e is the amount adsorbed at equilibrium (mg g⁻¹), k_1 is the pseudo-first order rate constant (min⁻¹) and t is the contact time (min).

Values of the constants, k_1 and q_e for the adsorption of dye on the adsorbents were determined from the slopes and intercepts of the plots $log(q_e - q_t)$ against t, respectively and their values are given in Table 4.

Pseudo-second order model can be represented in the following form

$$\frac{t}{q_t} = \frac{1}{k_2(q_e)^2} + \frac{C_e}{q_t} t \dots (7)$$

Where, k_2 is the Pseudo-second order rate constant (gmg⁻¹min⁻¹). The values of the q_e and k_2 were determined by potting a graph between t/qt and time.

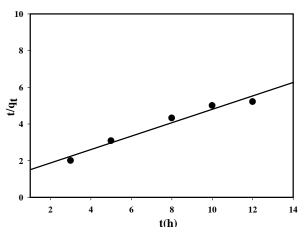


Figure 7. Pseudo- second order kinetics plot for the adsorption of Remazol Red on saw dust at 25°C.

Theoretical and experimental data for the adsorption kinetics are given in table 4. The experimental values of q_e are closer to the calculated values for second order kinetics than those of first order kinetics. The value of correlation coefficient (R^2) for second order is also closer to unity as compared to that of first order (Table 4). Therefore, the adsorption of selected dye on rice husk, sawdust and charcoal, more appropriately followed pseudo second order kinetic model.

 Table 4. Kinetic parameters for the adsorption of remazol red on sawdust.

1.1		q _e exp. mg/g	Pseudo second order kinetic model			
q _e (mg/g)	K_1 (h ⁻¹)	R ²	-	q _e (mg/g)	K ₂ (h , g/mg)	R ²
	2.62	0.83	2.36	2.73	0.092	0.96

Conclusion

In the present investigation activated saw dust was found to be better adsorbent for the removal of Remazol Red from aqueous media as compared to commercial charcoal. Adsorption of the investigated dye decreases with the increase in pH and slightly increases with temperature of the solution. It was observed that adsorption process followed pseudo-second order kinetic model. Values of qe calculated from pseudo second order plots are in good agreement with the experimental values. Future investigations should be conducted with a view to selectively separating the present dye contaminants, regenerating the exhausted biomass, recovering the sorbed dye and designing to continuous dye treatment systems. These studies can further ameliorate the economic aspects of dye wastewater treatment which will get better opportunity for the water related pollution remediation in pharmacology.

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